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Title	Acute biomechanical effects of a lightweight, sock-style minimalist footwear design during running; a musculoskeletal simulation and statistical parametric mapping approach
Type	Article
URL	https://clock.uclan.ac.uk/id/eprint/26437/
DOI	https://doi.org/10.1080/19424280.2019.1593516
Date	2019
Citation	Sinclair, Jonathan Kenneth, Brooks, Darrell and Stainton, Philip (2019) Acute biomechanical effects of a lightweight, sock-style minimalist footwear design during running; a musculoskeletal simulation and statistical parametric mapping approach. Footwear Science, 11 (2). pp. 71-83. ISSN 1942-4280
Creators	Sinclair, Jonathan Kenneth, Brooks, Darrell and Stainton, Philip

It is advisable to refer to the publisher's version if you intend to cite from the work.
<https://doi.org/10.1080/19424280.2019.1593516>

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Acute biomechanical effects of a lightweight, sock-style minimalist footwear design during running; a musculoskeletal simulation and statistical parametric mapping approach.

Abstract

The aim of this study was to examine the effects of existing minimalist footwear, new sock-style minimalist footwear and conventional running footwear on lower extremity biomechanics, using a musculoskeletal simulation and statistical parametric mapping (SPM) approach. Thirteen male participants ran over an embedded force plate at 4.0 m/s, in 1. existing minimalist footwear, 2. new sock-style minimalist footwear and 3. conventional running shoes. Kinematics of the lower extremities were collected using an eight-camera motion analysis system and lower extremity joint loading was also explored using a musculoskeletal simulation approach. Differences between footwear conditions were examined using SPM and one-way repeated measures ANOVA. The strike index indicated that the foot contact position was significantly more anterior in existing minimalist footwear (44.19 %) and new sock-style minimalist footwear (42.33 %) compared to conventional running shoes (29.00 %). The instantaneous loading rate was also significantly larger in existing minimalist footwear (271.68 BW/s) and new sock-style minimalist footwear (299.26 BW/s) in relation to conventional running shoes (122.48 BW/s). In addition, during the late stance phase compressive hip joint loading was significantly larger in both minimalist footwear. Similarly, Achilles tendon loading was statistically greater in both minimalist footwear compared to the conventional running shoe during the early and middle aspects of the stance phase. The observations from this analysis show that minimalist footwear may

place non-habituated runners at greater risk from the mechanical factors linked to the aetiology of chronic lower limb running related injuries.

Introduction

Running is one of the most popular aerobic exercise modalities, and there is an overwhelming body of evidence that it mediates a plethora of physiological and psychological benefits (Lee et al., 2014). However, running is also associated with an extremely high susceptibility to chronic pathologies; with up to 80 % of runners experiencing an injury each year (Van Gent et al., 2007). Chronic injuries are a key barrier to training compliance (Hespanhol et al., 2016), and result in a significant economic burden due to healthcare operation and absence from work (Junior et al., 2017).

As the primary interface between foot and ground, running shoes are proposed as a mechanism by which the rate of chronic injuries can be moderated (Shorten, 2000). However, since the introduction of the conventional running shoe in the 1970's, the rate and location of chronic running injuries has remained unchanged (Davis, 2014). This has led to the supposition that reverting to running in minimalist footwear that lacks the mechanical properties associated with the conventional running shoe, may be associated with a reduced incidence of chronic running injuries (Lieberman et al., 2010). Based on this supposition several minimalist footwear models such as the Vibram Five-Fingers are currently available commercially.

Several studies have explored biomechanical differences between minimalist and conventional running shoes. These analyses have typically examined spatiotemporal characteristics, lower limb kinematics and loading rates. Sinclair et al., (2013a) and Sinclair et al., (2016) showed that minimalist footwear caused runners to run with a more plantarflexed ankle at initial contact, increased peak tibial internal rotation and an increased vertical loading rate in comparison to conventional running shoes. Squadrone et al., (2009) similarly showed that running in minimalist footwear increased the ankle plantarflexion angle at footstrike but also reduced stride length and the impact peak of the vertical ground reaction force (GRF). Squadrone et al., (2015) investigated the effects of different minimalist footwear conditions via the strike index. Their findings showed that minimalist footwear mediated a midfoot strike pattern, with alterations being most pronounced in footwear with the least midsole cushioning. Sinclair et al., (2018) showed that the strike index did not change between different minimalist footwear models and conventional running shoes, but did find that effective mass was significantly larger in minimalist footwear with alterations again being more evident in models with the least midsole cushioning.

Previous work has also examined the effects of minimalist footwear on the loads experienced by the lower extremities joint during running. Sinclair, (2014) and Sinclair et al., (2016) showed that peak patellofemoral stress was significantly reduced in minimalist footwear, but peak Achilles tendon loads were significantly increased. Similarly, Bonacci et al., (2018) showed that peak patellofemoral stress was significantly lower in minimalist footwear. In addition, Sinclair, (2016) showed that peak tibiofemoral loading did not differ significantly between minimalist and conventional footwear during running. Furthermore, Sinclair et al., (2015) and Sinclair et al., (2016) taking into account the effect of changing stride length examined the effects of different minimalist footwear. Patellofemoral impulse per mile was

71 significantly reduced but Achilles tendon impulse per mile was significantly greater in
72 minimalist footwear, with differences being more evident in minimalist footwear with the
73 least midsole cushioning. Recently, a new lightweight, sock-style minimalist footwear design
74 has been commercially released, which represents an extremely lightweight sock style upper
75 with a strong abrasion resistant sole. There are however, no published scientific
76 investigations concerning this new footwear, indicating that examination of running
77 biomechanics whilst wearing these shoes is warranted.

78
79 Previous analyses concerning the biomechanical differences between minimalist and
80 conventional footwear, have utilized mathematical modelling approaches driven by joint
81 torques to explore the loads experienced by the musculoskeletal system. However, joint
82 torques are global indices of joint loading, and therefore not representative of localized joint
83 loading (Herzog et al., 2003a). Herzog et al., (2003b) identified importantly that the muscles
84 are the primary contributors to lower extremity joint loading. Due to the difficulties
85 associated with calculating muscle kinetics, the role of the muscles in controlling joint
86 biomechanics during running has received little attention within biomechanical literature.
87 Over the past decade however, significant advances have been made in improving
88 musculoskeletal models; leading to the development of open access and bespoke software.
89 Allowing skeletal muscle forces to be simulated during movement, and utilized as inputs to
90 calculate lower extremity joint reaction forces (Delp et al., 2007). Such approaches have not
91 yet been utilized to explore biomechanical differences between minimalist and conventional
92 running shoes.

To date biomechanical differences between minimalist and conventional footwear have been explored statistically through extraction of discrete kinetic/ kinematic parameters. This approach can however be limiting, as it can lead to potentially relevant information being discarded (Warmenhoven et al., 2018). Therefore, Statistical parametric mapping (SPM) may represent an efficacious supplement to discrete analyses, as it is able to compare an entire time normalized data series (Pataky et al., 2013). To date there has yet to be any biomechanical investigation, which has examined the effects of different minimalist footwear and conventional running shoes on the biomechanical parameters linked to the aetiology of running injuries using SPM.

To summarize, there is currently no scientific research concerning the aforementioned sock-style minimalist footwear, nor is there any investigation which has collectively explored the effects of minimalist and conventional running shoes using both musculoskeletal simulation and SPM. Therefore, the aim of the current investigation was to examine the effects of existing/ sock-style minimalist footwear and conventional running shoes on lower extremity biomechanics using a musculoskeletal simulation and SPM based approach. A study of this nature may provide further insight into the biomechanical differences between minimalist and traditional running shoes; particularly with regards to runners' predisposition to chronic running injuries.

Methods

Participants

Thirteen male runners volunteered to take part in this study. This sample size is commensurate with previous analyses concerning the biomechanics of running in minimalist

footwear (Sinclair et al., 2013a; Sinclair et al., 2015). The mean characteristics of the participants were: age 27.31 ± 3.50 years, height 1.73 ± 0.04 m and body mass 72.23 ± 5.66 kg. The procedure utilized for this investigation was approved by the University of Central Lancashire, Science, Technology, Engineering and Mathematics, ethical committee. All runners were free from musculoskeletal pathology at the time of data collection. Participants provided written informed consent in accordance with the principles outlined in the Declaration of Helsinki.

Footwear

The footwear used during this study consisted of New Balance, 1260 v2 (New Balance, Boston, Massachusetts, United States; henceforth termed Shoe A), Vibram Five-Fingers, ELX (Vibram, Albizzate, Italy; henceforth termed Shoe B) and Skinners, Athleisure (Skinners Technologies, Cyrilka, Czech Republic; henceforth termed Shoe C) (Figure 1). Shoe A had an average mass of 0.285 kg, heel thickness of 25 mm and a heel drop of 14 mm. Shoe B had an average mass of 0.167 kg, heel thickness of 7 mm and a heel drop of 0 mm. Finally, Shoe C had an average mass of 0.08 kg, heel thickness of 6 mm and a heel drop of 0 mm. The footwear were also scored using the minimalist index described by Esculier et al., (2015), and Shoe A received a score of 20, Shoe B a score of 92 and Shoe C a score of 100.

@@@ Figure 1 near here @@@

Procedure

Participants ran at 4.0 m/s ($\pm 5\%$), striking an embedded piezoelectric force platform (Kistler Instruments Ltd., Winterthur, Switzerland) with their right foot. Running velocity was monitored using infrared timing gates (Newtest, Oy Koulukatu, Finland). The stance phase was delineated as the duration over which 20 N or greater of vertical GRF was applied to the force platform. Runners completed a minimum of five successful trials in each footwear condition. As each footwear were novel to all participants, a period of 5 minutes for accommodation was allowed. This involved running through the testing area without concern for striking the force platform (Sinclair et al., 2013a; Sinclair et al., 2016). The order that participants ran in each footwear condition was counterbalanced. Kinematic and GRF data were synchronously collected. Kinematic data were captured at 250 Hz via an eight-camera motion analysis system (Qualisys Medical AB, Goteburg, Sweden). Dynamic calibration of the motion capture system was performed before each data collection session.

Lower extremity segments were modelled in 6 degrees of freedom using the calibrated anatomical systems technique (Cappozzo et al., 1995). To define the anatomical frames of the thorax, pelvis, thighs, shanks and feet retroreflective markers were placed at the C7, T12 and xiphoid process landmarks and also positioned bilaterally onto the acromion process, iliac crest, anterior superior iliac spine (ASIS), posterior superior iliac spine (PSIS), medial and lateral malleoli, medial and lateral femoral epicondyles, greater trochanter, calcaneus, first metatarsal and fifth metatarsal. Carbon-fibre tracking clusters comprising of four non-linear retroreflective markers were positioned onto the thigh and shank segments. In addition to these, the foot segments were tracked via the calcaneus, first metatarsal and fifth metatarsal, the pelvic segment was tracked using the PSIS and ASIS markers and the thorax segment was tracked using the T12, C7 and xiphoid markers. Static calibration trials (not normalized to

static trial posture) were obtained in each footwear allowing for the anatomical markers to be referenced in relation to the tracking markers/ clusters.

Processing

Dynamic trials were digitized using Qualisys Track Manager (Qualisys Medical AB, Goteburg, Sweden) in order to identify anatomical and tracking markers then exported as C3D files to Visual 3D (C-Motion, Germantown, MD, USA). All data were linearly normalized to 100 % of the stance phase. GRF data and marker trajectories were smoothed with cut-off frequencies of 50 Hz at 12 Hz respectively, using a low-pass Butterworth 4th order zero lag filter. All force parameters throughout were normalized by dividing by bodyweight (BW).

In accordance with the protocol of Addison & Lieberman, (2015), an impulse-momentum modelling approach was utilized to calculate effective mass (% BW), which was quantified in accordance with the below equation:

$$\text{Effective mass} = \text{vertical GRF integral} / (\Delta \text{foot vertical velocity} + g * \Delta \text{time})$$

The impact peak was defined in Shoe A as the first peak in vertical GRF. In Shoes B and C where no impact peak was present, according to the protocols of Lieberman et al., (2010) and Sinclair et al., (2018) we defined the position of the impact peak at the same relative position as in Shoe A, which was shown to be 11.96 % of the stance phase. The time (ms) to impact peak (Δtime) was quantified as the duration from footstrike to impact peak. The vertical GRF

187 integral (BW·ms) during the period of the impact peak was calculated using a trapezoidal
188 function. The change in foot **vertical** velocity ($\Delta foot\ vertical\ velocity$) was determined as the
189 instantaneous vertical foot velocity averaged across the 10 frames prior to the impact peak
190 **(Sinclair et al., (2018))**. The velocity of the foot was quantified using the centre of mass of the
191 foot segment in the vertical direction, within Visual 3D (Sinclair et al., 2018).

192
193 **Instantaneous loading rate (BW/s) was also was also extracted by obtaining the peak increase**
194 **in vertical GRF between adjacent data points.** Finally, the strike index was calculated as the
195 position of the centre of pressure location at **footstrike**, relative to the total length of the foot
196 (Squadrone et al., 2015). A strike index of 0–33% denotes a rearfoot, 34–67% a midfoot and
197 68–100% a forefoot strike pattern.

198
199 Following this, data during the stance phase were exported from Visual 3D into OpenSim 3.3
200 software (Simtk.org). A validated musculoskeletal model with 12 segments, 19 degrees of
201 freedom and 92 musculotendon actuators (Lerner et al., 2015) was used to estimate lower
202 extremity joint forces. The model was scaled to account for the anthropometrics of each
203 athlete. As muscle forces are the main determinant of joint compressive forces (Herzog et al.,
204 2003), muscle kinetics were quantified using static optimization in accordance with Steele et
205 al., (2012). Compressive patellofemoral, medial/ lateral tibiofemoral and hip joint forces were
206 calculated via the joint reaction analyses function using the muscle forces generated from the
207 static optimization process as inputs. **Finally, Achilles tendon forces were estimated in**
208 **accordance with the protocol of Almonroeder et al., (2013), by summing the muscle forces of**
209 **the medial gastrocnemius, lateral, gastrocnemius, and soleus muscles.**

Running in minimalist footwear has been shown to alter step length during running (Sinclair et al., 2016), which increases the number of footstrikes necessary to run a set distance. We therefore firstly calculated hip, tibiofemoral, patellofemoral and Achilles tendon impulse during the stance phase, using a trapezoidal function. In addition to this, we also estimated the total impulse per kilometre ($BW \cdot km$) by multiplying these parameters by the number of steps required to run a kilometre. The number of steps required to complete one kilometre was quantified using the step length (m), which was determined by taking the difference in the horizontal position of the foot centre of mass between the right and left legs at footstrike.

Statistical analyses

Compressive joint forces (hip, patellofemoral, medial tibiofemoral and lateral tibiofemoral), Achilles tendon loading and three-dimensional kinematics during the entire stance phase were temporally normalized using linear interpolation to 101 data points. Differences across the entire stance phase were examined using 1-dimensional SPM with MATLAB 2017a (MATLAB, MathWorks, Natick, USA), in accordance with Pataky et al., (2016), using the source code available at <http://www.spm1d.org/>. In agreement with Pataky et al., (Pataky et al., 2013), SPM was implemented in a hierarchical manner, analogous to one-way repeated measures ANOVA (SPM F) with post-hoc paired t-tests (SPM t). Therefore, the entire data set was examined first, and if a statistical main effect was reached, then post-hoc tests were conducted on each component separately.

For discrete parameters that could not be examined using SPM (hip impulse per km, lateral impulse per km, medial impulse per km, patellofemoral impulse per km, Achilles tendon impulse per km, step length, instantaneous load rate, strike index and effective mass), means

and standard deviations were calculated for each outcome measurement for all footwear conditions. Differences in discrete biomechanical parameters between footwear were examined using one-way repeated measures ANOVAs, Effect sizes were calculated using partial η^2 ($p\eta^2$). In the event of a significant main effect, post-hoc pairwise comparisons were conducted on all significant main effects, using a Bonferroni adjustment. Discrete statistical actions were conducted using SPSS v24.0 (SPSS Inc., Chicago, USA). Statistical significance for main effects was accepted at the $P \leq 0.05$ level (Sinclair et al., 2013b).

Results

@@@ Figure 2 near here @@@

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@@@ Table 1 near here @@@

Lower extremity external loading, strike index and step length

A main effect was revealed for the instantaneous **loading** rate ($P < 0.001$, $p\eta^2 = 0.75$). Post-hoc analyses showed that instantaneous **loading** rate was significantly larger in Shoe B ($P < 0.001$) and Shoe C ($P < 0.001$), compared to Shoe A (Table 1).

A main effect was shown for strike index ($P = 0.033$, $p\eta^2 = 0.27$). Post-hoc analyses showed that strike index was significantly larger in Shoe B ($P = 0.008$) and Shoe C ($P = 0.006$), compared to Shoe A (Table 1).

A main effect was evident for effective mass ($P=0.005$, $\eta^2 = 0.38$). Post-hoc analyses showed that effective mass was significantly larger in Shoes A ($P=0.01$) and C ($P=0.04$), compared to Shoe B (Table 1). Finally, a main effect was shown for step length ($P=0.012$, $\eta^2 = 0.33$). Post-hoc analyses showed that step length was significantly larger in Shoe A compared to Shoe C ($P=0.005$) (Table 1).

Joint loading per kilometre

At the hip joint a main effect was found for peak hip impulse per kilometre ($P=0.018$, $\eta^2 = 0.31$). Post-hoc analysis showed that hip impulse per kilometre was significantly larger in Shoe C compared to shoe A ($P=0.004$) (Table 1).

There was also a main effect for patellofemoral impulse per kilometre ($P=0.029$, $\eta^2 = 0.28$). Post-hoc analysis showed that patellofemoral impulse per kilometre was significantly larger in Shoe C compared to shoe B ($P=0.02$) (Table 1).

Finally, a main effect was found for Achilles tendon impulse per kilometre ($P<0.001$, $\eta^2 = 0.58$). Post-hoc analyses showed that Achilles tendon impulse per kilometre was significantly larger in Shoes B ($P=0.001$) and C ($P=0.002$) compared to shoe A (Table 1).

Statistical parametric mapping - joint loading

@@@ Figure 4 near here @@@

279 **@@@ Figure 5 near here @@@**

280 **@@@ Figure 6 near here @@@**

281
282 At the hip joint, there was a significant main effect (Figure 4a). Post-hoc analyses showed
283 that Shoe A was associated with lower compressive hip force than Shoes B and C, from 82-
284 88% of the stance phase (Figure 4bc).

285
286 At the patellofemoral joint, there was a significant main effect (Figure 4d). Post-hoc analyses
287 showed that Shoe A was associated with lower patellofemoral force than Shoe B from 81-
288 90% of the stance phase (Figure 4e).

289
290 At the medial aspect of the tibiofemoral joint, there was also a main effect (Figure 4f). Post-
291 hoc analyses showed that Shoe A was associated with lower compressive force than Shoe B
292 from 5-10% and 80-92% of the stance phase (Figure 4g). In addition, Shoe A was associated
293 with lower compressive loading than Shoe C from 5-10% of the stance phase yet greater
294 loading from 4-9% of the stance phase (Figure 4h).

295
296 At the lateral aspect of the tibiofemoral joint, there was also a main effect (Figure 5a). Post-
297 hoc analyses showed that Shoe A was associated with lower compressive force than Shoe B
298 82-89% of the stance phase (Figure 5b). In addition, Shoe A was associated with lower
299 compressive force than Shoe C, between 0-3% of the stance phase (Figure 5c).

At the Achilles tendon, there was a main effect (Figure 5d). Post-hoc analyses showed that Shoe A was associated with lower tendon loading than Shoe B, between 7-12%, 17-55% and 82-92% of the stance phase (Figure 5e). In addition, Shoe A was associated with lower tendon loading compared to Shoe C, from 0-3%, 20-25% and 35-50% of the stance phase (Figure 5f).

Statistical parametric mapping - three-dimensional kinematics

For tibial internal rotation, there was a main effect (Figure 5g). Post-hoc analyses showed that Shoe A was associated with **increased** tibial internal rotation than Shoe B, between 0-5% and 90-100% of the stance phase (Figure 5h).

At the ankle in the sagittal plane, there was a main effect (Figure 6a). Post-hoc analyses showed that Shoe A was significantly more dorsiflexed than Shoe B, from 0-3% of the stance phase (Figure 6b). In addition, it was revealed that Shoe A was significantly more dorsiflexed than Shoe C, from 0-8% of the stance phase (Figure 6c).

Discussion

The current investigation aimed to examine the effects of existing/ sock-style minimalist footwear and conventional running shoes on lower extremity biomechanics using a musculoskeletal simulation and SPM based approach. To the authors knowledge this is the first investigation to comparatively examine these footwear and to explore the biomechanics of running in conventional and minimalist footwear using musculoskeletal simulation and SPM.

324

325 The kinematic analysis using SPM showed that the ankle was in a significantly more
326 plantarflexed position during the early stance phase in Shoes B and C in comparison to Shoe
327 A. This observation is reinforced by the discrete point analysis of the strike index, which
328 showed that the contact position was significantly more anterior in Shoes B and C, and a
329 midfoot strike pattern was adopted when wearing these footwear. This finding concurs with
330 the observations of Sinclair et al., (2013a) and Sinclair et al., (2016) who each showed an
331 altered foot position when wearing minimalist footwear. It is proposed that this relates to the
332 absence of cushioning in Shoes B and C, causing runners to adopt a flatter foot position in
333 order to compensate for the lack of midsole interface in an attempt to attenuate the load
334 experienced by the lower extremities (Lieberman et al., 2010).

335

336 The findings from the current investigation also showed that the instantaneous loading rate
337 was significantly larger and the effective mass was significantly lower in Shoes B and C
338 compared to Shoe A. This observation agrees with those of Sinclair et al., (2013a) and
339 Sinclair et al., (2016) but opposes those of Squadrone & Gallozzi, (2009) and Sinclair et al.,
340 (2018). Transient loading is governed by the rate at which the momentum of the foot
341 changes, therefore midsole material at the foot-ground interface strongly influences the
342 magnitude of transient forces during running (Whittle, 1999). Importantly, Addison &
343 Liebermann, (2015) found that the loading rate and effective mass were inversely associated
344 during running. Therefore, the aforementioned observation in relation to the loading rate is
345 supported by the effective mass observations, which was shown to be reduced in Shoes B and
346 C compared to Shoe A. Given the proposed association between the instantaneous rate of
347 loading and the aetiology of chronic injuries, this finding may be clinically meaningful,

(Milner et al., 2006), and indicates that Shoes B and C may place runners at increased risk from impact related injuries compared to Shoe A.

At the hip joint, the current investigation showed using SPM, that Shoe A significantly reduced compressive hip joint loading during the early and late aspects of the stance phase compared to Shoes B and C. This observation is supported through the discrete point analysis, which showed that compressive joint forces experienced per kilometre were statistically greater in Shoe C compared to shoe A. As the current investigation represents the first investigation to compare hip joint loading when running in minimalist and conventional footwear using musculoskeletal simulation, comparisons in relation to previous analyses are not possible. Nonetheless, the results are partially supported by those of Rooney & Derrick, (2013) and Sinclair, (2018) who showed that modifying the foot position significantly enhanced compressive hip joint loading during running. As the aetiology of hip joint pathologies are strongly influenced by compressive hip joint loading (Johnson & Hunter, 2014), the current investigation indicates that Shoes B and C may increase runners' susceptibility to chronic hip pathologies.

A further important observation from the current analysis is that patellofemoral loading contrasted using SPM was statistically larger in Shoe B compared to Shoe A during late stance. The discrete analysis differed from this, showing that patellofemoral force per kilometre was significantly larger in Shoe C compared to shoe B. The observations from the current investigation oppose those of Sinclair, (2014), Sinclair et al., (2016) and Bonacci et al., (2018) who showed significant reductions in peak patellofemoral stress and patellofemoral impulse per mile when running in minimalist footwear. This observation may

be due to the mechanism by which patellofemoral forces were calculated, as previous utilized mathematical models have not accounted for muscular co-contraction, and Sinclair, (2018) similarly showed using musculoskeletal simulation that running barefoot did not attenuate patellofemoral kinetics compared to conventional running shoes. The current investigation indicates firstly that running in minimalist footwear may not necessarily attenuate the magnitude of patellofemoral loading linked to the aetiology of patellofemoral disorders during running, in relation to conventional running shoes. Furthermore, the current study revealed that patellofemoral was statistically larger in Shoe C compared to shoe B, indicating that despite their relatively similar design characteristics (Esculier et al., 2015); Shoe C may place runners at increased risk from patellofemoral chronic injuries.

At the medial and lateral tibiofemoral joint compartments, compressive loading was significantly greater in Shoes B and C in relation to Shoe A, during the early and late aspects of the stance phase. This observation opposes those of Sinclair, (2016) but is supported closely by those of Sinclair, (2018); who showed that the medial and lateral tibiofemoral compressive rate of loading was statistically greater when running barefoot. This observation may be clinically meaningful, as increased compressive loading at both aspects of the tibiofemoral joint, is recognised as the primary risk factor in relation to the aetiology and progression of osteoarthritic symptoms (Dabiri & Li, 2013). Therefore, the current study shows that indicates that running in minimalist footwear may increase runners predisposition to the risk factors linked to the initiation of tibiofemoral osteoarthritis.

The findings from the current investigation also revealed using SPM that Achilles tendon loading was statistically larger during the mid and late aspects of the stance phase in Shoes B

and C compared to Shoe A. In addition, the discrete point analysis of tendon loading per kilometre similarly indicated that Shoes B and C were associated with statistically larger tendon loading magnitudes. This observation concurs with those of Sinclair, (2014) and Sinclair et al., (2015) who similarly showed that peak Achilles tendon force and tendon impulse per mile were greater when running in minimalist footwear in comparison to conventional running shoes. The aetiology of Achilles tendinopathy is associated with excessive and repeated tendinous loading, during cyclic activities such as running (Magnusson et al., 2010). Excessive tendon loading without sufficient caseation of running activities between training sessions, mediates collagen and extracellular matrix synthesis and degradation of the tendon (Magnusson et al., 2010). As such, the current investigation shows that running in minimalist footwear may place runners at increased risk from the biomechanical parameters linked to Achilles tendinopathy, in comparison to conventional running shoes.

A potential limitation that should be acknowledged in regards to the current investigation is of course that only runners who habitually ran in conventional running shoes were examined. The findings from previous analyses concerning the biomechanics of minimalist footwear and conventional running shoes have drawn opposing interpretations, frequently on the basis of the running experience of the participants in minimalist footwear (Sinclair et al., 2013a; Squadrone & Gallozzi, 2009). It can therefore be ventured that the findings from the current investigation may have been different, had the participants been habitual minimalist footwear users. As such, future analyses using musculoskeletal simulation and SPM investigating the biomechanics of running in habitual minimalist footwear is recommended, allowing more decisive assertions in regards to the aetiology of chronic pathologies to be drawn.

420

421 In conclusion, though the biomechanics of running in minimalist and conventional running
422 footwear have received widespread research attention, there has not yet been a quantitative
423 comparison of lower extremity biomechanics in minimalist and conventional running shoes
424 using a musculoskeletal simulation and SPM based approach. This study revealed that the
425 instantaneous load rate, hip, tibiofemoral and Achilles tendon force parameters were
426 statistically larger when running in Shoes B and C compared to Shoe A. Therefore, the
427 observations from this analysis show that minimalist footwear may place non-habituated
428 runners at greater risk from the mechanical factors linked to the aetiology of chronic lower
429 limb running related injuries.

430

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Figure 1: Experimental footwear (A = New Balance/ Shoe A, B = Vibram Five-Fingers/ Shoe B and C = Skinnners/ Shoe C).

Figure 2: Hip, knee and ankle kinematics in the a. sagittal, b. coronal and c. transverse planes as a function of footwear (black = Shoe A, dash = Shoe B and grey = Shoe C), (FL = flexion, AD = adduction, IN = inversion, INT = internal, EXT = external).

541 Figure 3: Lower extremity joint loading as a function of footwear (black = Shoe A, dash =
542 Shoe B and grey = Shoe C), (a. = hip, b. = patellofemoral, c. = medial tibiofemoral, d. =
543 lateral tibiofemoral and e. Achilles tendon).

544 Figure 4: Statistical parametric mapping results in relation to lower extremity joint loading (a.
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549 Figure 5: Statistical parametric mapping results in relation to lower extremity joint loading
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